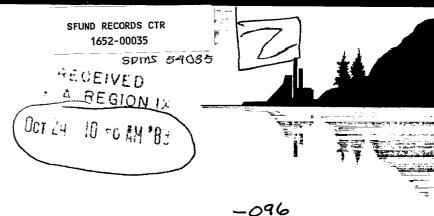
Pan Canadian Consultants Limited

1040 - 999 Suite 424 - 882 West Hastings Street Vancouver British Columbia XXXX V6C 1M3 (604) 688-8618

Environmental and et gincorma consultants to manishy and government



12 October 1983

United States Environmental Protection Agency Region IX 215 Fremont Street San Francisco, CA 94105 U.S.A.

Attn: Mr. Harry Seraydarian, Director, Toxics & Waste Management Division.

Dear Sir,

We were requested recently by Mr. C. N. Thodos, President of Ruskin Developments Ltd., to provide you with copies of data we had collected during the project work we undertook for Ruskin on the Iron Mountain property. Some of the paperwork in our files is not relevant to your investigation, so we have sorted out the information that may be useful.

The enclosures are:

- our final report to Ruskin (which contains much earlier data in the appendices)
- copies of chemical analyses on acid mine drainage, and on treated water samples (after our tests).

We do not possess any other information that would be useful to your investigation. We understand that Ruskin will be asking their geological consultant to forward data relating to the geology of the area.

Please confirm that you have received this information.

Yours truly

PAN CANADIAN CONSULTANTS LIMITED

W. B. Alderton, P.Eng.,

President.



test Itd.

1523 WEST 3rd AVENUE, VANCOUVER, B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

Report On	Analysis of solution samples	File No	1298F
-		Report No.	•
Reported To	C. G. Environmental Engineering	P.O. #	
	5583 Spruce St.	Date	July 26, 1983
	Burnaby, B.C. V5G 1Y7		
Attention:	Dr. C. Guarnaschelli, P. Eng.		

We have tested the samples submitted by you on July 18, 1983 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled as given on the following Plasma Certificates.

METHOD OF TESTING:

Prior to analysis the samples were digested using an ultra pure nitric acid. The resulting solutions were then analyzed for metals using an Inductively Coupled Argon Plasma Spectrograph.

RESULTS OF TESTING:

See attached Plasma Certificate.

Richard S. Jorni

Supervisor

Trace Netals Laboratory

/cs



test itd.

1523 WEST 3rd AVENUE, VANCOUVER. B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

To: C. G. Environmental Engineering

PLASMA SPECTROGRAPHIC ANALYSIS CERTIFICATE

5583 Spruce St.

File No. 1298F

Burnaby, B.C. V5G 1Y7

Date July 26/83

Attention:

Dr. C. Guarnaschelli, P. Eng.

The hereby Certify that the following are the results of plasma spectrographic analysis made on __solution__ samples submitted.

Me hereby Cer	rlify that t	he following are t	he results of plass	ma spectrographi	c analysis made o	n	samples submitted.
Sample Identificati	on	10/Superna- tant 3.2	10/superna- tant 3.9	·	Compsite As veceved	ppt 3.9	
Newholisch w NAOH to	pH—	≯ }.√	3.9	4.2	Rijinal Sample	Shudge from pH 39.	Detection Limit
Aluminum Antimony Arsenic Barium Beryllium Bismuth Boron Cadmium Calcium Chromium Cobalt Copper Iron Lead Magnesium Manganese Mercury Molybdenum Nickel Phosphorus Potassium Selenium Silicon Silver Sodium Strontium	Al Sb As Ba Be Bi BCCa Cr Co Cu Fe Mg Mn PO ₄ Kse SiO ₂ Na Sr	742. L 0.10 L 1.25 129. 4850. 0.89 413. 12.6 - L 0.35 9.93 60.1 - 134. L 2310.	556. L 0.067 L 1.18 119. 4230. 0.71 412. 12.6 - L 0.33 4.64 60.5 - 112. L 3320. 0.21	594. L L 0.027 L L 4.41 131. L 1.19 119. 4530. 1.00 421. 12.8 - L 0.37 6.14 60.1 - 117. L 3240. 0.22	763. L L 0.020 L L 4.32 133. L 1.16 133. 5510. 1.25 428. 12.9 - L 0.34 13.6 '49.3 - 126. L 53.4 0.18	117. L 1.52 189. 11800. 4.00 382. 11.1 - L 0.45 46.6 57.8 - 225. L 2910. 0.25	1.5 1.5 3.0 0.01 0.03 5.0 0.10 0.25 0.10 0.30 0.20 0.15 0.30 0.80 0.01 0.03 - 0.40 0.25 4.0 0.1 - 0.8 0.10 0.25
Tin Titanium Tungsten Uranium Vanadium	Sn Ti W U V	L 0.13 1.19	0.11 - - 0.39	0.11 - - 0.50	1.23	-	0.30 0.06 - - 0.10 0.15
Zinc	Zn	606.	607.	626.	631.		L

All results expressed in parts per million.

L = fess than.

Plasma 1

1



test Itd.

Report On	Analysis of solution samples	File No	0987F	_
Reported To	C. G. Environmental Engineering			_
	5583 Spruce St.		June 20, 1983	
	Burnaby, B.C. V5G 1Y7			
Attention:	Dr. C. Guarnaschelli, P. Eng.			

We have tested the samples submitted by you on June 15, 1983 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled as given on the following Plasma Certificates.

METHOD OF TESTING:

Prior to analysis the samples were digested using an ultra pure nitric acid. The resulting solutions were then analyzed for metals using an Inductively Coupled Argon Plasma Spectrograph.

RESULTS OF TESTING:

See attached Plasma Certificate.

10/1 1/

Richard S/ Jo Supervisor

Trace Metals Laboratory

/cs





1523 WEST 3rd AVENUE, VANCOUVER, B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

To:
 C. G. Environmental Engineering

PLASMA SPECTROGRAPHIC ANALYSIS CERTIFICATE

5583 Spruce St.

File No. 0987F

Burnaby, B.C. V5G 1Y7

Date June 20/83

Attention:

Dr. C. Guarnaschelli, P. Eng.

Me hereby Certify that the following are the results of plasma spectrographic analysis made on solution samples submitted.

Sample Identification		Composite #1	Supernatant #1 pH 5.5	NaS Supernatant #2		
		Mixture of Briles of Stidwede	Newhalised Litt NaOH	After Nass alked.		Detection Limit
Aluminum Antimony Arsenic Barium Beryllium	Al Sb As Ba Be	674. L 13.0 L L	4.48 L L 0.013 L	L L L 0.36		1.5 1.5 3.0 0.01 0.03
Bismuth Boron Cadmium Calcium Chromium	Bi B Cd Ca Cr	L 4.50 6.20 119. L	L L 5.18 106. L	L L L 57.4 L		0.10 0.25 0.10 0.30
Cobalt Copper Iron Lead Magnesium	Co Cu Fe Pb Mg	L 154. 7260. 2.50 394.	L 4.36 5180. <u>L</u> 346.	L 0.080 2120. L 185.		0.20 0.15 0.30 0.80 0.01
Manganese Mercury Molybdenum Nickel Phosphorus	Mn Hg Mo Ni PO ₄	11.4 - L 0.29 15.3	10.1 - L L 8.74	5.26 - L L		0.03 - 0.40 0.25 4.0
Potassium Selenium Silicon Silver Sodium	K Se SiO ₂ Ag Na	29.4 - 129. L 31.6	22.6 - 33.2 L 4140.	16.5 - 16.7 L 4400.		0.1 - 0.8 0.3 1.0
Strontium Tin Titanium Tungsten Uranium	Sr Sn Ti W U	0.13 L 1.14	0.19 L 0.12 -	0.10 L 0.13		0.01 0.30 2.5 -
Vanadium Zinc	V Zn	1.02	L 598.	L 132.		0.10 0.15

All results expressed in parts per million.

L = less than.

Plasma 1

CANTEST LTD.

Spéctroscopist



ENVIRONMENTAL LABORATORY 2218 RAILROAD AVENUE, P.O. BOX 2088 REDDING, CA 96001—TELEPHONE (916) 243-5831 REF. NO. 9230DATE 6/21/83PAGE 1 OF 2

Piiysical Chemical & Bacteriological Analysis

SPECIFIC ANALYSIS

525 M	arket St.			
ATTN: Bill	AldertoN		_ PHONE:	
		ie		
DATE OF SAMPLE_	6/14/83	_ DATE RECEIVED	6/14/83	<u> </u>
TESTS	B in=Boulder Ck. Plant Influent	B lgry out=Boulder Plant Primary cell		t=Boulder Ck.Plant effluent
pH (units)	1.20	1.33	N	1.33
Total Dissolved Solids	57720	59870		55320
Copper	166	13.6		5.17
Total Iron	11,300	13,100		13,200
Ferrous Iron	5160	6520	W.	6670
Zinc	1050	1060	1050	52.3
Ferric Iron (by calculation)	6140	6580		6530
COMMENTS: Result	s are in milligrams p	per liter unless othe	rwise noted	

The information shown on this sheet is test data only and no analysis or interpretation is intended or implied.

Bacteriological, and Bioassay Examinations

Form 65



ENVIRONMENTAL LABORATORY 2218 RAILROAD AVENUE, P.O. BOX 2088 REDDING, CA 96001-TELEPHONE (916) 243-5831

9230 REF. NO 6/21/83

Physical Physical Chemical & **Bacteriological Analysis**

SPECIFIC ANALYSIS

TION Iron Moun	tain Mine DATE RECEIVED _	SAMPLED BY: client
		0/ 14/ 03
	S in=Slickrock Ck. plant influent	S out=Slickrock Ck. plant effluent
	2.59	2.62
	10490	10130
	122	122
	1210	1230
	477	474
	49.1	50.0
)	733	756
ılts are in mill	igrams per liter unless oth	nerwise noted.
on	on)	plant influent 2.59 d 10490 122 1210 477 49.1

State Approved Water Laboratory for Chemical, Bacteriological, and Bioassay Examinations

The information shown on this sheet is test data only and no analysis or interpretation is intended or implied.

Form 65

THE IRON MOUNTAIN PROPERTY

REPORT ON WORK PROGRESS AND DISCUSSIONS WITH GOVERNMENT AGENCIES

PAN CANADIAN CONSULTANTS LIMITED

VANCOUVER

Bic. Angust Final Nepal Aday 83

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APPENDICES

Appendix l	-	Proposed Superfund Program for Iron Mountain
Appendix 2		Press Release regarding Fine on IMMI
Appendix 3	-	Memo dated 30 June 1983
Appendix 4		Proposal submitted to WQCB and EPA
Appendix 5		Typical Precious Metal Values in AMD

1. INTRODUCTION

Pan Canadian Consultants Limited were retained by Ruskin in April 1983 to assist them in resolving problems at the Iron Mountain mine at Redding, California. Tasks assigned to Pan Canadian included:

- Task 1 establish good relations with the appropriate government agencies to relieve pressure on Ruskin and to overcome some of the problems created by previous owners of the property.
- Task 2 examine the acid mine drainage (AMD) at Iron
 Mountain to see if a feasible and economic
 process could be developed to extract
 metals values from the AMD.
- Task 3 determine how best the environmental problems at Iron Mountain could be resolved.

We have completed our work as far as we can at this time. Further work will depend on Ruskin's decision whether to proceed with property acquisition or to drop the property.

This brief report summarises our findings to date, and should give Ruskin some guidance on whether it should continue with the property. As discussed in our meeting of 2nd August 1983, and further in this report, continuance with the project will require Ruskin to make a committment to spend considerable sums of money to satisfy the various government agencies.

2. TASK 1 - Government Relationships

We believe that Ruskin has now developed an excellent relationship with the Environmental Protection Agency (EPA) and the Regional Water Quality Control Board (WQCB). Our meetings with these agencies have convinced them that Ruskin is serious about solving the problems at Iron Mountain. The government personnel realize that the problems are no fault of Ruskin's and they have a great deal of sympathy for Ruskin's position.

However, the Iron Mountain environmental problems have continued unresolved for so long that the EPA is not willing to delay its planned studies using "Superfund" money at all. Work is scheduled to commence this month and will be completed in about 12 months. The only way that the government will back-out is if Ruskin and/or IMMI agrees to do the proposed work (or an agreed alternative) itself. The proposed EPA work program is attached as Appendix 1.

The attached work program is to be undertaken by CH₂M-Hill of Redding and will cost about \$600,000 (U.S.).* Once the work has been done, the EPA will try to obtain its refund from the "responsible" parties.

We have tried to involve the EPA with Ruskin in a shared cost program, but the EPA is not prepared to do this. The work will be done on an ALL or NOTHING basis i.e. either Ruskin puts up all the money or the EPA will. However, all EPA Superfund monies are claimable back from the responsible party

We estimate the cost at about \$300,000 (CAN) if Pan Canadian did the work for Ruskin.

2.1 Superfund Program

The attached work program is to be completed by U.S. consultants in the next 12 months, and will cost about \$600,000 (U.S.). Once it has been completed, the EPA will seek to recover this money from the responsible parties. Therefore, if Ruskin continues to be involved with the property, it will be held partly liable. If Ruskin does continue with the property, it makes more sense for Ruskin to do the work itself, since it would mean a saving of about \$350,000 (CAN).

If Ruskin abandons the Iron Mountain property, it cannot held liable for return of the EPA Superfund money, and this responsibility would revert to IMMI and possibly to previous owners of the property.

The large amounts of money involved with the recent fine imposed on IMMI (Appendix 2) and with the Superfund program, have a significant effect on the feasibility of the entire project, and Ruskin should carefully evaluate whether it wishes to remain involved with the property. Since none of the problems with the property are of Ruskin's making, it would seem that all these costs should be borne by IMMI.

It must be realized that the Superfund work program will be commencing in August 1983, and expenditure will be made at the rate of about \$50,000 (U.S.) per month. This expenditure will continue unless Ruskin decides to take over the work program itself. Funds expended, plus additional costs for program administration, interest, etc., will be recovered by EPA

These extra costs may be substantial.

Since Ruskin does not yet know if it will continue with the project, and since Ruskin does not want to waste money, we suggest that further work be limited to the minimum necessary to retain good relations with the government agencies until Ruskin can make a decision on the property.

3. TASK 2 - Extraction Process.

In our memo of 30th June 1983 (Appendix 3) and in the July proposal to the WQCB and EPA (Appendix 4), we discussed alternative methods for treating AMD to recover saleable metals. We eliminated several potential processes from consideration because of various technical problems. Apart from the cementation process, now used in the Boulder and Slickrock Creek plants to recover copper, we felt that the use of a sulphide preferential-precipitation process showed promise in producing a marketable copper/cadmium sulphide product. Initial laboratory results were encouraging, although iron precipitation was also occurring at the pH value we used for sulphidation (pH 5.5).

More recent tests at lower pH values (pH 3.2, 3.9, 4.2) show that co-precipitation of iron is still a major problem even though theoretically it should not be. The problem is severe enough to rule out the sulphide process as a feasible method for the recovery of saleable metals. The problem occurs because of the very high concentration of dissolved iron (0.5-0.7%) in the AMD compared with the concentrations of other metals. It therefore seems that only the existing cementation process is an economical method of treating AMD for copper removal.

Initially, we were given analyses showing appreciable dissolved gold and platinum in the AMD. Subsequent examination of analyses done by others, and check analyses run by ourselves, show that no such precious metal values occur. Typical values are shown in Appendix 5. The loss of these precious metals removed much of the incentive from our work, since only the gold and platinum seemed to offer a significant opportunity to make a profit. Base metal recovery from AMD is not profitable.

In conclusion, there does not appear to be a suitable economical method for recovering saleable product from the AMD except copper cementation with iron.

4. TASK 3 - Environmental Control.

4.1 Proposed Program

The work program proposed by the EPA (Appendix 1) is designed to produce the most economical solution to the environmental problems caused by Iron Mountain AMD. The ideal solution would be to eliminate all AMD, and this possibility will be examined. However, assuming that AMD continues into the future, treatment will be necessary to reduce the pollution entering the Sacramento River. From our studies, and from work done by many other researchers, we believe the most economical treatment will be neutralisation with lime/limestone and precipitation of the metals as hydroxides. This process is conventional and proven, and has been tested on the Iron Mountain AMD by CH₂M-Hill.

The process will involve directing all AMD to a central point, neutralising with lime/limestone, and settling

in large ponds. Clear decant liquor will be discharged to the river. Sludge will be dredged out from time-to-time and buried in a landfill. The plant and pond area likely will be several miles away from the mine site on the flats to the west of the Sacramento River. AMD will be delivered there via a pipeline.

The cost of constructing the plant and settling ponds will probably be \$1-1½ million (U.S.). Operating and maintenance costs will be in the order of \$500-750,000 (U.S.) per year (1983 dollars). There will be no possibility of any economic return to offset these costs. Treatment, and hence the on-going operating costs, will have to be continuous for as long as AMD is produced from the mine.

Responsibility for constructing and operating the treatment facility will rest with the owner(s) and/or operator(s) of the Iron Mountain Property. This is a cost factor that should be given careful consideration when making a decision on the viability of the Iron Mountain project.

4.2 Alternative Programs.

As discussed in our July proposal (Appendix 4), it may be possible to reduce or eliminate the flow of AMD by a number of methods. These include:

- a) reinjecting AMD into the mine workings.
- b) intercepting groundwater flows before they can enter the workings.
- c) keeping the Brick Flat pit pumped out or at a very low level.
- d) preventing surface water from entering the mine.
- e) sealing mine openings to prevent AMD discharge.

A preliminary cost estimate of \$48,500 was given for a trial of alternative a) in our July proposal.

Alternative c) would cost about \$15,000 for capital installation plus about \$10,000 per year for operating/maintenance costs. If c) is to be implemented it should be this summer while the Brick Flat pit is dry.

No costs have been developed for b) and d); extensive geotechnical studies would be required. We believe that alternative e) has only a slight chance of success, since there are so many potential openings that could drain the mine.

Since these alternatives could cost substantial amounts of money, it does not make much economic sense for Ruskin to implement them unless it is committed to the property.

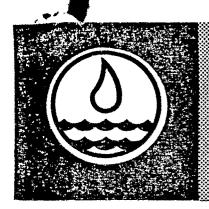
5. CONCLUSIONS

Until Ruskin makes a decision regarding the feasibility of the Iron Mountain property, it should minimize its expenditures on the environmental aspects. We suggest that a low level of effort be maintained in keeping in touch with the WQCB and with EPA - possibly 1-2 days per month of Mr. Alderton's time. Other expenditures should be held in abeyance until such time as a decision has been made to proceed with acquisition of the property. At that time, Ruskin should advise the agencies that it proposes to do the remedial work itself. If Ruskin decides not to purchase the property, then no cost penalty will be incurred by not doing the work at this time i.e. Ruskin will not be liable for reimbursing the EPA for the money spent under the Superfund program.

APPENDIX 1

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APPENDIX 2



CALIFORNIA RECIONAL WATER OUALITY CONTROL

CORTRO EOARD

CENTRAL VALLEY REGION

100 E. CYPRESS AVENUE

REDDING, CALIFORNIA

96002

Mr. James Pedri, Supervising Engineer

26 July 1983

** FOR IMMEDIATE RELEASE **

The State of California and the owners of Iron Mountain Mine have reached settlement in their long standing lawsuit.

In a stipulation signed Wednesday by Justice Frances N. Carr sitting in the 3rd District Court of Appeals in Sacramento, Iron Mountain Mines, Inc. agreed to pay the state \$500,000.00 for violations of the California Water Code. The Central Valley Regional Water Quality Control Board has maintained that Iron Mountain Mines, Inc. failed to operate existing copper removal facilities according to state standards. The judgment may be reduced to \$400,000.00 if Iron Mountain Mines, Inc. begins making payment to the state within 30 days and continues to pay at least \$75,000.00 per year for the next five years.

"Although the settlement amount is somewhat less than the original judgment, the \$400,000.00 represents the largest settlement for water pollution in this state, and probably the nation, against an abandoned or nonoperating business," said James Pedri, Supervising Engineer with the Board's Redding office. James Pedri also added that, "the judgment is only for past violations of the Board's orders and in no way relieves Iron Mountain Mines, Inc. of their responsibility to clean up toxic discharges from their property."

The Regional Water Quality Control Boards, State Department of Health
Services and Environmental Protection Agency are pursuing the use of "Superfund"
money to study and clean up the pollution problem. A work plan has recently

been approved in Washington to spend over \$600,000.00 in the next several months to complete all necessary studies. "We foresee the start of major cleanup activities sometime next summer," said Mr. Pedri. According to federal law, Iron Mountain Mines, Inc. will be responsible for repaying the state and federal government for all costs associated with the Superfund cleanup.

Iron Mountain Mines, Inc. may still be able to avoid high cleanup costs if they are successful in developing an operating mine on their property.

Ruskin Developments, Ltd., a canadian mining company, has leased the mineral rights to Iron Mountain Mines, Inc.

If current testing by Ruskin indicates sufficient mineral value, then the mines can again be operated at a profit. Such operation will allow for recovery, treatment or elimination of existing toxic mine discharges.

#

APPENDIX 3

Memo to: Tyke Thodos Date: 30 June 1983

from: Bill Alderton

Subject: Summary of the Iron Mountain Acid Drainage Problem

and Possible Methods of Treatment.

The problem

The Water Quality Control Board (WQCB) has identified 18 sources of acid mine drainage (AMD) within the Iron Mountain area. However, they are mainly interested in only 4 major discharges. These are:

- 1. Richmond portal
- 2. Lawson portal
- 3. Slickrock Creek seep
- 4. Old #8 portal

#1 and 2 are now combined and flow to the Boulder Creek cementation plant via a pipeline and trough. #4 is now collected and directed to the Slickrock Creek plant. #3 discharges into Slickrock Creek untreated, although it could be collected and sent to the plant.

Flow rates are not monitored, although there is a V-notch weir at the outfall from the Boulder Creek plant (this is now calibrated and Frank Foster should be taking readings daily). The WQCB has measured flows from time to time. Based on their results I have assumed that mean annual flows for the above sources are:

3 + 4 = 800 l/min (180 gpm)

Since flow measurement equipment is just being installed, it is impossible to verify these flows. However, they are a useful starting point for discussion. Flow measurements will be taken on a regular basis in future, so we can check my assumptions.

From numerous WQCB analyses, I have derived an average analysis for Boulder Creek and Slickrock Creek plant influents. These are:

Parameter	Boulder Ck	Slickrock Ck
рн	1.3	2.5
Cu	250 mg/l	150 mg/l
Zn	1300 "	70 "
Cđ	10 "	0.5 "
Fe	12000 "	1500 "

I have also assumed that there is a silver content of 0.19 mg/l in both waters, although this is based on only one analysis (D'Appolonia, 1981). More recent analyses by CH₂M-Hill show silver values of only 0.02-0.09 mg/l.

Using the above flows and analyses, the maximum possible metal recovery from the AMD is:

Cu	195 MT/yr	= \$300,300 @ 70¢/lb
Zn	713 "	= \$533,324 @ 34¢/1b
Cd	5½ "	= \$7,260 @ 60\$/1b
Fe	6860 "	Zero value
Ag	180 Kg	= \$ 88,700 @ \$14/oz
Total		\$929,584

I assume that there is no market for iron. In practice, the actual \$ recovery may be less than \$500,000/yr - this depends to some extent on the quality of the extracted metals.

An earlier analysis showed dissolved gold and platinum in the drainage. I am having analyses done to check this out, but discussions with both the WQCB and CH₂M-Hill in Redding tend to discount the possibility of precious metals in the water. You may remember also, that I expressed doubts about this when we first met; gold and platinum do not dissolve readily in water or sulphuric acid.

Apart from the economics of recovering metals values, there is the problem of pollution control and the need to satisfy the WQCB. This must be dealt with even if no economic return is possible. We are examining methods for treating the AMD and you will soon have a copy of a proposal to the WQCB for EPA Superfund \$. We are trying to concentrate the metals so that we can remove them as cheaply as possible.

Some processes are clearly unsuitable or technically unfeasible. Others show promise but need more work. The processes considered are described in the following sections.

Demineralization by Ion Exchange.

Ion exchange demineralizers have been demonstrated to treat successfully a synthetic AMD, and to produce potable water. (Holmes & Kreusch, 1972). Their tests however, used AMD with much lower concentrations of dissolved constituents than occur at Iron Mountain. A comparison of AMD quality is shown below:

		Concentration	(mg/l)
	Holmes &	Kreusch	Iron Mountain (Boulder Ck Plant)
Acidity (as CaCO ₃)	500		Est 20,000
Sulphate	1150		47,000
Ca	200		. 66
Mg	24		720
Al	15		1,550
Fe	210		8,700
Cu	0		130
Zn	0		1,300

The difference in the total dissolved solids makes the process of ion exchange impossible to justify unless there are ion exchange resins capable of selectively adsorbing Cu, Zn, and Cd in preference

to iron and aluminum. At present there do not appear to be such resins. Without these resins, one cubic foot of standard ion exchange resin will treat only about 12 gallons water before it requires regeneration. This is unacceptable since it would make the cost of ion exchange excessive.

Ion exchange demineralisation would be so uneconomic that it cannot be considered any further.

Reverse Osmosis (R.O.)

R.O. is an established technology used widely in the production of industrial process water and drinking water from brackish or sea-water. It has also been demonstrated to treat AMD successfully in the U.S. (Wilmoth, 1973).

Use of R.O. would produce one fairly pure stream (permeate) that could be discharged to surface streams without further treatment, and a concentrated stream (reject) that would contain almost all dissolved minerals originally in the AMD. It would thus concentrate the water to allow treatment in smaller facilities and to enhance metal recovery.

We have discussed R.O. with Seagold Industries in Vancouver, and with Fluid Systems Division of U.O.P. in San Diego (U.O.P. makes R.O. units). U.O.P. have a couple of systems working on AMD streams but not as acidic or as concentrated as at Iron Mountain.

U.O.P. advise that their R.O. membranes cannot handle the acidity of the Iron Mountain AMD, and also that they would be concerned about membranes fouling with iron, manganese and gypsum. They suggested neutralising to pH 8-9 to remove iron and manganese before running the neutralised and clarified effluent through a R.O. unit. Since the U.O.P. R.O. units are believed to be more resistant to fouling than other types (because of their construction) we have assumed that other R.O. systems will have even more problems with the Iron Mountain AMD.

The requirement for neutralisation makes the use of R.O. units impractical. At pH 8-9 most of the dissolved solids in the AMD will be removed as hydroxides and gypsum and there would be no need to use R.O. Adding a R.O. unit to treat already neutralised water would cost over \$1,000,000 and would not achieve any great improvement. There would be no economic return.

For these reasons, R.O. is not a feasible trearment for the Iron Mountain AMD. No further work is planned.

Neutralisation with lime or limestone

The addition of lime (Ca(OH)₂) or limestone (CaCO₃) to AMD will neutralise the acidity and result in the removal of dissolved metals as hydroxide precipitates. At pH 8-9 most of the dissolved metals can be removed, leaving about 0.5-1.0 mg/l in the neutralised decant liquid and most of the metals in the precipitated sludge.

Unfortunately, in the case of Iron Mountain, the AMD contains high concentrations of sulphate ion. Addition of calcium ion will give a massive precipitate of gypsum (CaSO₄). This will form 60-70% of the final sludge volume. Iron and aluminum hydroxides will form another 30-35% of the final sludge volume. The marketable metals (Cu, Zn, Cd) will only comprise about 5% of the total sludge volume.

This "dilution" by gypsum, iron and aluminum renders the produced sludge unsaleable, and means that neutralisation with lime/limestone is a "throw-away" process involving the continual use of large quantities of chemicals, the continual need to dispose of large volumes of sludge, and the impossibility of ever realising any cost recovery from sale of a product.

The WQCB has contracted a company in Redding (CH₂M-Hill) to study the lime/limestone process. They have just completed their pilot-plant work at the Boulder Creek plant site. Their initial results

indicate that a settled sludge volume of about 20% of the original AMD volume is produced. Based on a combined flow rate of 1800 1/min (400 gpm) the annual sludge production will be almost 7 million cubic feet (260,000 cubic yards). CH₂M-Hill are proposing that the sludge be concentrated by evaporation in summer, so that the total solids volume would be reduced. Nevertheless, the volume to be landfilled or ponded is still considerable.

Lime/limestone neutralisation is a proven process that will solve the pollution problem. It has no other redeeming features and must be considered as a last resort if all else fails. This process has not been rejected but is being ignored for the moment while we examine an alternative.

Partial neutralisation and sulphide addition

Metallic sulphides are almost totally insoluble in neutral or alkaline waters. Their solubility increases in acid waters, but is still low at pH 3-5.

Partial neutralisation to pH 3-5 using an alkali plus a sulphide (eg Na₂S) will precipitate most of the metals as sulphides without contaminating them with gypsum. Subsequent neutralisation with lime to pH 8 and aeration will remove most of the iron and sulphates in a separate stage where they will not contaminate the metallic sulphides. The objective of this 2-stage process is to allow the recovery of a fairly pure mixture of CuS, ZnS and CdS for sale to a smelter.

The disadvantage of sulphide precipitation is that the cost of chemicals is higher than lime and limestone. On the other hand, recovery of the metal sulphides offsets these costs and may result in an overall lower treatment cost. Until some more experimental work has been done to optimise the chemical dosages it is impossible to conclude what the costs of sulphidation will be.

The partial neutralisation/sulphidation process is being examined for its practicability on Iron Mountain AMD. Further small-scale work is continuing and will be reported in future. This process is the subject of our proposal to the WQCB for EPA Superfund money to do some pilot-plant work on site (see proposal for details).

Recirculation of AMD back into the mine

As has been mentioned in your offices, the possibilty of pumping AMD back into the mine may increase the concetration of copper to the point where electrowinning is possible. I think we will find that the volume of water leaving the portals will increase steadily if we do this, but I will come up with some cost estimates for installing the necessary pump, pipeline and well. I have included this option in the proposal to the WQCB for partial financing by the EPA.

Interception of groundwater and pumping

It seems to me that much of the water infiltrating the old workings and causing the AMD originates as ground water - possibly from some distance away from the mine. If this is the case, it should be possible to install water wells and pumps to draw down the water table around the mine area, and to prevent water from entering the mine workings. An alternative would be to re-enter the mine and to seal points where water flows in. I doubt if the mine is safe enough to enter to do this type of work, so it really boils down to intercepting flows before they can reach the mine.

This approach has much to recommend it. Once the initial expense of well/pump installations has been incurred, the operating costs

will be relatively low - just power for the pumps. If successful, the AMD would cease totally and there would be no need for any treatment facilities. Of course, there would never be any economic return either.

This alternative would require a major geotechnical investigation of groundwater conditions around the mine. Existing drill holes may provide useful data if piezometers can be installed in them. I do not have a handle on the \$ involved with this course of action. I have included it in our proposal only at a preliminary stage, and have suggested that you would want to discuss it with the WQCB.

EPA "Superfund" availability

The EPA has promised about \$800,000 to study the Iron Mountain problem. Discussions have already taken place between the EPA, WQCB and the State Department of Health Services to establish terms-of-reference for the study; the contractor will be CH₂M-Hill.

The WQCB is assuming that Ruskin will not go through with the purchase of the Iron Mountain property and that, therefore, the State will have to develop a solution to the problem. If Ruskin was operating the mine, you would be expected to do the work.

The results of the Superfund contract will not necessarily be imposed on Ruskin by the WQCB, but once a process or method has be arrived at, pressure will be put on Ruskin to implement a solution at least equal to the WQCB's.

The importance of the problem and the potential high costs involved make it desirable for Ruskin to keep a close liaison with the authorities in California; in particular the WQCB. It would also be most desirable for Ruskin to have a direct involvement with the Superfund work, by way of doing a joint program with government.

The WQCB suggested that we submit a proposal for Superfund money to study the problem, and to examine the proposed sulphidation process in detail. It will be necessary for Ruskin to propose a joint funding approach because I am sure that the EPA will not agree to 100% funding. The split I have used is 50/50.

The proposed program is described in a separate proposal - you have a copy.

APPENDIX 4

PROPOSAL FOR A STUDY OF THE FEASIBILITY OF TREATING IRON MOUNTAIN ACID MINE DRAINAGE

RUSKIN DEVELOPMENTS LTD VANCOVER B.C.

Propose submitted to EPA & WOCD.

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Figure 1 - Possible plant conversion - Alternative 1
Figure 2 - Possible plant conversion - Alternative 2
Schedule

INTRODUCTION.

The Iron Mountain mine at Redding produces large volumes (est. 300 - 500 gpm) of acid mine drainage (AMD) year-round. The AMD has a low pH (1 - 3.5) and contains high concentrations of dissolved copper, zinc, iron and aluminum, together with appreciable quantities of manganese and cadmium. Dissolved sulphate concentrations have been measured as high as 47,000 mg/l.

The origin of the AMD is meteoric water, and possibly groundwater, infiltrating the old workings of the mine and ore bodies via fractures and old adits. Once inside the mine, bacterial activity converts sulphides to sulphuric acid which dissolves the metallic constituents of the ore. The residence time and reaction rate in the mine are unknown. Evidence that vigourous reactions are taking place is provided by a number of old portals that "steam", by the fact that drainage from the Richmond portal is quite warm, and by the extremely high dissolved solids concentrations (over 20,000 mg/l) in the drainage.

At present, drainage from the three largest sources is treated in small cementation plants to remove dissolved copper. These plants use scrap steel to precipitate the copper, while releasing a large concentration of iron into solution. The drainage is then allowed to discharge into Slickrock Creek and Boulder Creek, both tributary to Spring Creek. A number of smaller seeps discharge into the Spring Creek system untreated. Spring Creek flows are regulated by a dam at the Spring Creek Generating Station, and water is discharged into the Keswick reservoir on the Sacramento River.

The Spring Creek discharge has been determined to be detrimental to the water quality of the Sacramento River downstream from the Keswick reservoir, and fish mortality has been recorded (D. Heiman. pers. comm.). Since the Sacramento River is used by spawning

chinook salmon, the potential exists for damage to this resource via toxicity from heavy metals dissolved in the river water and from suspended particulate materials, mainly ferric hydroxide, which can interfere with respiration by coating the gills.

As a result of these concerns, Iron Mountain Mines Inc. was required to limit the discharge of copper from its operations and to ensure that receiving water quality in the Keswick reservoir or Sacramento River did not exceed certain specified levels (California Regional Water Quality Control Board Order Nos. 77-225 and 78-152).

Ruskin Developments Ltd. is considering the purchase and renewed operation of the Iron Mountain property. As such, it wishes to resolve some of the past problems associated with this property and is prepared to use its best efforts to limit the extent of AMD production and to develop a process to treat AMD. To meet these objectives Ruskin has engaged a consulting company (Pan Canadian Consultants Limited) to study the problem and to recommend a suitable course of action.

The consultant has studied the alternatives available for treatment of the AMD and reports that only two methods appear feasible. These are:

- 1. the lime/limestone process currently under investigation by CH₂M-Hill
- 2. a partial neutralisation/sulphidation process to precipitate metals as sulphides

The second process appears to have the potential to make a partial economic return, while reducing heavy metal levels below those possible with hydroxide precipitation.

The consultant, having done some laboratory-scale experiments, wishes to proceed to a pilot-plant scale to verify that the proposed process does allow preferential precipitation of heavy metal sulphides under larger-scale conditions, and to permit the development of capital and O & M costs for a process.

The consultant has also considered the possibility of preventing the creation of AMD by limiting the inflow of water into the . mine workings, and by recirculating AMD back into the mine to develop an in-situ leaching operation. These possibilities are discussed later in this proposal.

Ruskin is willing to enter into a joint funding venture with government to ensure that adequate finances are made available to examine these important potential methodologies for solving the problem at Iron Mountain. Since the proposed treatment methodology has already been examined to some degree by the consultant, and since Ruskin is prepared to match the contribution by government on a 50/50 basis, we believe that the government would obtain a more cost-effective and economical use of its funds by participating jointly on this program with Ruskin. The present consultants for Ruskin would undertake the work, and would report to both parties to the agreement. Details of funding are discussed in a later section of the proposal.

STUDY OBJECTIVES

The objectives of the proposed work are:

- to develop a feasible method for the removal of heavy metals from AMD
- 2. to obtain better water discharge quality than can be obtained from other alternative treatment(s)
- 3. to attempt to obtain a marketable product from the process to offset its operating costs and, if possible, to make an operating profit

- 4. to add to the knowledge and understanding of AMD treatment technology, and to develop procedures that may be applicable elsewhere
- 5. to examine the potential for "zero discharge" of mine water by recirculation of AMD back into the workings, or of interception of groundwater flows before they can infiltrate the mine workings.

Ruskin believes that the approach suggested by the consultant is logical and should be examined further. Initial results indicate the potential for high efficiency waste treatment and the discharge of high quality effluent using sulphide precipitation. The potential for closed-loop circulation of AMD back into the mine has not been examined in the same detail but has great merit, since it may solve the problem of AMD discharge at source.

TECHNICAL PROPOSAL

A number of potential processes have been examined to treat the AMD. Those considered are:

Ion exchange

Rejected because of the high TDS of the AMD, the low treatment capacity of available resins (@30 kgr/ft³, 1 ft³ of resin will treat only about 12 gallons AMD before exhaustion), and the potential for severe iron and manganese fouling of the resins. Operating costs would be excessive and waste regenerants would pose a significant waste disposal/treatment problem of their own.

Reverse osmosis

Rejected because of the low pH and the potential for iron, manganese and calcium sulphate fouling. UCP Fluid Systems advised that their spiral-wound membranes would not be able to operate in the low pH conditions at Iron Mountain unless the water was first neutralised to raise its pH and to precipitate iron. Since this would by itself solve most of the problem, the addition of R.O. would then be pointless.

Neutralisation with lime/limestone

This is being researched by CH₂M-Hill under contract with the WQCB. Neutralisation to pH 8-9 with aeration of ferrous to ferric hydroxide will remove metals down to acceptable levels. Disadvantages of the process are that there is no prospect of any economic return, the large areas required for sludge settling ponds, and the fact that metallic hydroxides tend to redissolve under acidic conditions. This process is considered as a "last resort" if the proposed alternative processes and procedures fail to meet our expectations.

The process we propose taking to the pilot stage is discussed in the following sections.

Partial neutralisation and treatment with sulphides.

Chemical background

The basic premise behind the proposed process is that metallic sulphides are much less soluble than metallic hydroxides.

Typical solubility products for metallic compounds (Ref 1) are:

CuS
$$1 \times 10^{-40}$$
 Cu (OH) $_2$ 6×10^{-20} ZnS 1×10^{-23} Zn (OH) $_2$ 1×10^{-17}

MnS	1×10^{-16}	Mn (OH) 2	4×10^{-14}
CdS	1×10^{-28}	Cd (OH) 2	1×10^{-14}
FeS	1×10^{-22}	Fe (OH) $\frac{1}{2}$	1×10^{-15}
		Fe (OH) 3	1×10^{-38}

(these values are not quoted as being precise but are of order of magnitude).

Equally as significant as the low solubility of the metallic sulphides is the fact that they are insoluble at relatively low pH levels. Thus, at pH 4, solution concentrations of CuS, ZnS and CdS would not exceed 0.10 mg/l. By comparison, most hydroxides require a pH of 8-9 for effective removal. (Zn(OH)₂ has a minimum solubility at pH 9-10; Cd(OH)₂ has a minimum solubility at pH 11). Furthermore, metal hydroxides will redissolve readily when the pH is lowered, as can occur in tailings ponds over time. The amount of metal redissolving increases with decreasing pH.

The ability to precipitate metal sulphides at low pH permits the selective separation of metals. Neutralisation with soda ash or caustic will limit the precipitation of calcium sulphate or ferric hydroxide and will retain a fairly clear solution. Addition of a sulphide (BaS, Na₂S, NaHS) will selectively precipitate the heavy metal sulphides as a dense sludge which can be reclaimed, dewatered and sold.

Following heavy metal removal, the solution can be aerated to remove excess sulphide ion and treated further with lime or limestone with aeration to precipitate iron as Fe(OH)₃ and aluminum. After settling, the supernatant liquid would be discharged to surface waters. The ferric and aluminum hydroxides/calcium sulphate sludge could be ponded or possibly filtered to dry-haul to a disposal site.

The process has been demonstrated by numerous researchers (Ref 2,3,4) and in the laboratory by our consultants. They

are now at the stage where pilot-scale work is needed to optimise the treatment process.

Pilot study

It is proposed to operate a pilot-plant at the Boulder Creek plant site. The unit would comprise 2-3 reaction vessels and a number of settling tanks. The reactors would each be 50-100 gallons capacity. Initially the pilot-plant would operate batch-wise to establish parameters for optimum operation (pH, sulphide concentration, reaction times, settling rates etc) but would subsequently be arranged to operate continuously for short periods.

The first reaction vessel would be for initial pH adjustment. The second reactor would be for sulphide addition. The contents of the second reactor would be drained into a settling tank after sulphide addition. The third reactor would be used for final neutralisation and aeration.

The pilot study will concentrate on establishing and optimising basic parameters for a full-scale plant. These include:

- the minimum pH level for initial neutralisation to permit complete removal of heavy metals in the second stage without contamination with Fe(OH)₃
- optimisation of sulphide dosage
- sludge settling rates, composition and filterability
- effectiveness of aeration for sulphide removal
- decant neutralisation and aeration for ferric hydroxide precipitation

- ferric hydroxide/calcium sulphate sludge settling rate, composition, dewatering characteristics and filterability

Pilot-plant work is proposed to lead to a second stage study at a small plant scale.

Small plant scale study

Initial study of the existing Boulder Creek cementation plant indicates that the concrete cells could be cleaned out and converted to a sulphide precipitation plant with minor modifications. This preliminary evaluation is dependent on the conclusions reached during the prior pilot-plant work, but we believe that there is some evidence to show that the heavy metal sulphides will precipitate rapidly and that the Boulder Creek plant cells have the capacity and residence time to permit their complete separation and removal.

Post-sulphide neutralisation and ferric hydroxide precipitation may also be possible; this will be examined during the pilot-plant study.

A possible conversion of the Boulder Creek plant and an operational flowsheet is shown on Figure 1. Conversion will involve the cutting of some channels to interconnect cells, the installation of mixers, feeders, small chemical feed tanks, aerators, pumps and a small filtration unit.

Cell dimensions, volumes and residence times for a 150 gpm flow are given below:

Initial neutralisation cell; 5' x 10' x 35' 1750 ft³
Residence 87 minutes

Rapid mix cell; 6' $\times 10$ ' $\times 4$ ' 240 ft³

Residence 12 minutes.

Sulphide settling basin; $30' \times 35' \times 4'$

4200 ft³

Residence 209 minutes

Neutralisation/aeration cell(each); $5' \times 8' \times 33'$ Flow 75 gpm/cell x 2 cells 1320 ft³

Residence 132 minutes

Sludge settling basins(each); $5' \times 8' \times 33'$ 50 gpm/cell x 3 cells 1320 ft^3

Residence 197 minutes

In the event that the 2-stage neutralisation/sulphidation process is found to be unfeasible or excessively costly to operate, the Boulder Creek plant may be convertible to a neutralisation/aeration plant with copper removal via iron cementation. This alternative is shown on Figure 2. Brief discussions with CH₂M-Hill personnel, and the data presented in the CH₂M-Hill progress report dated May 6, 1983, indicates that the metallic hydroxide/calcium sulphate sludge from lime/limestone neutralisation settles freely and is essentially completely settled after 2 hours. The existing plant cells will provide settling times of this order.

Recirculation of AMD to the mine workings.

The consultant is examining the possibility of collecting AMD from the Richmond and Lawson portals, pumping it through a pipeline up the mountain, and reinjecting the water through a well into the mine workings.

A location for the well site is presently under review. The objective of this particular course of action will be to try to concentrate dissolved metals in the AMD to a point where electrowinning of economic amounts of copper are possible. Ultimately, there is the possibility that AMD discharge could be halted entirely. The consultants will be developing cost estimates for this process in the near future. Costs presented in this proposal are preliminary.

Interception of groundwater flows

The Brick Flat pit has been pumped out, yet there has been no decrease in the quantity of AMD flowing from the Richmond and Lawson portals. The decline in AMD discharge over the past several months seems to relate more to the fact that the weather is drier, and little rainfall has occurred. The Slickrock Creek discharge from the Old #8 portal continues unabated.

These observations may be an indication that most water inflow to the mine workings originates as groundwater, possibly from aquifers some distance from the mine site. If this is the case, it may be possible to intercept groundwater flows with wells and to pump them before they can reach the workings. The supposition that the water source may be groundwater is not in disagreement with observed AMD flows, since the regional water table will be elevated during the winter rainy season and would tend to discharge more water into the mine. Conversely, the dry summer weather will lower the water table, and the amount of water that can invade the workings will be less.

This is an aspect of AMD control that Ruskin would like to explore further with government, since the implications of massive pumping of groundwater are considerable. No costs have been developed for this possible course of action. Ruskin is prepared to discuss similar conditions as for the other actions.

COST PROPOSAL

Ruskin Developments proposes entering into an agreement with the appropriate government agencies to provide 50% of the funds required to undertake the work outlined in this proposal. It is proposed that the work would be undertaken by Pan Canadian Consultants Limited personnel, and invoices, progress reports, draft and final reports would be submitted by the consultant to the WQCB for approval. Invoices and progress statements would be submitted monthly. Following approval, payment would be divided equally between Ruskin and government. Total cost for the work would not exceed that given in this proposal without prior approval by both parties.

Ruskin is prepared to enter into a formal agreement to legalise the arrangement.

COST ESTIMATE

a) Pilot-plant work

Material and equipment purchase	\$ 5,000
Equipment rental	\$ 5,000
Professional fees (est. 120 MD)	\$25,000
Travel, accommodation, misc. expenses	\$ 4,000
Sub-total - pilot-plant work	\$39,000

b) Plant-scale work

Plant alterations	\$ 8,000
Equipment Purchase	\$15,000
Equipment rentals	\$10,000
Chemicals and consumable supplies	\$ 1,500
Professional fees (est 180 MD)	\$38,000
Travel, accommodation, misc. expenses	\$ 5,000
Sub-total - Plant-scale work	\$77 , 500

TOTAL ESTIMATED COST (a+b) \$116,500

Preliminary cost estimate - recirculate AMD to mine:

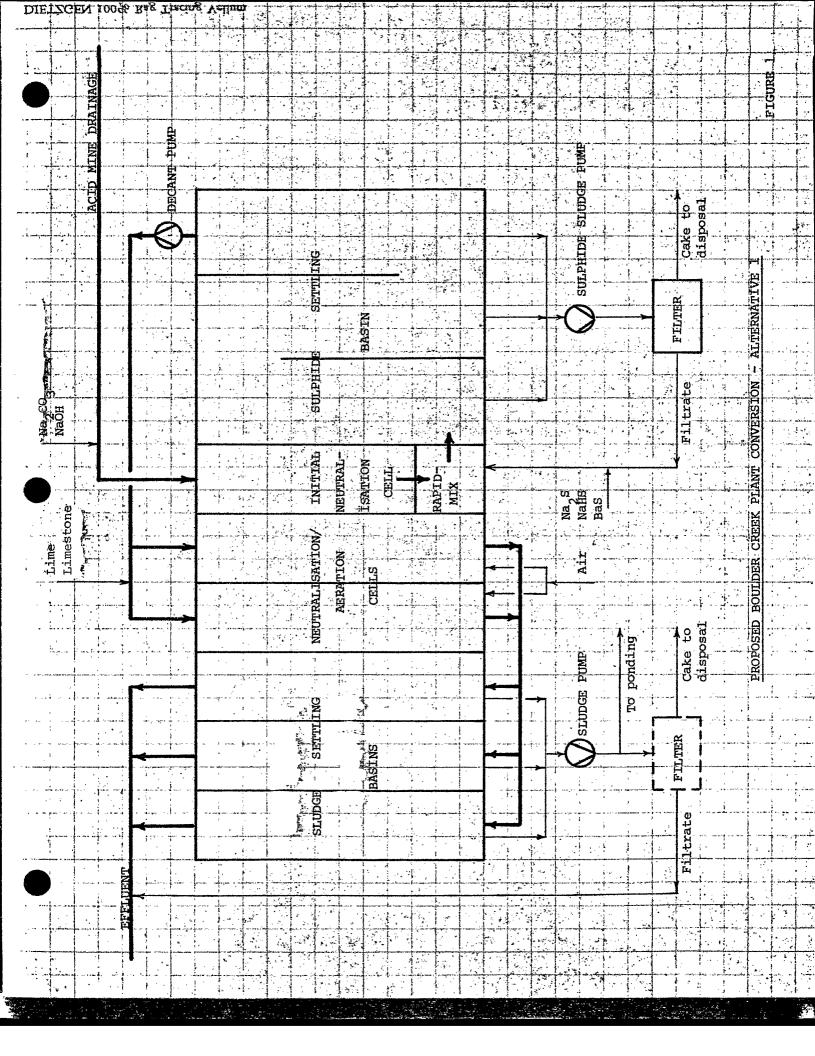
Pump purchase and installation	\$12,000
Pipeline (est 2000' @ 2" O.D.)	\$15,000
Well drilling/casing	\$ 8,000
Valves and fittings	\$ 5,000
Professional fees (est 20 MD)	\$ 6,500
Expenses	\$ 2,000
Estimated cost	\$48,500

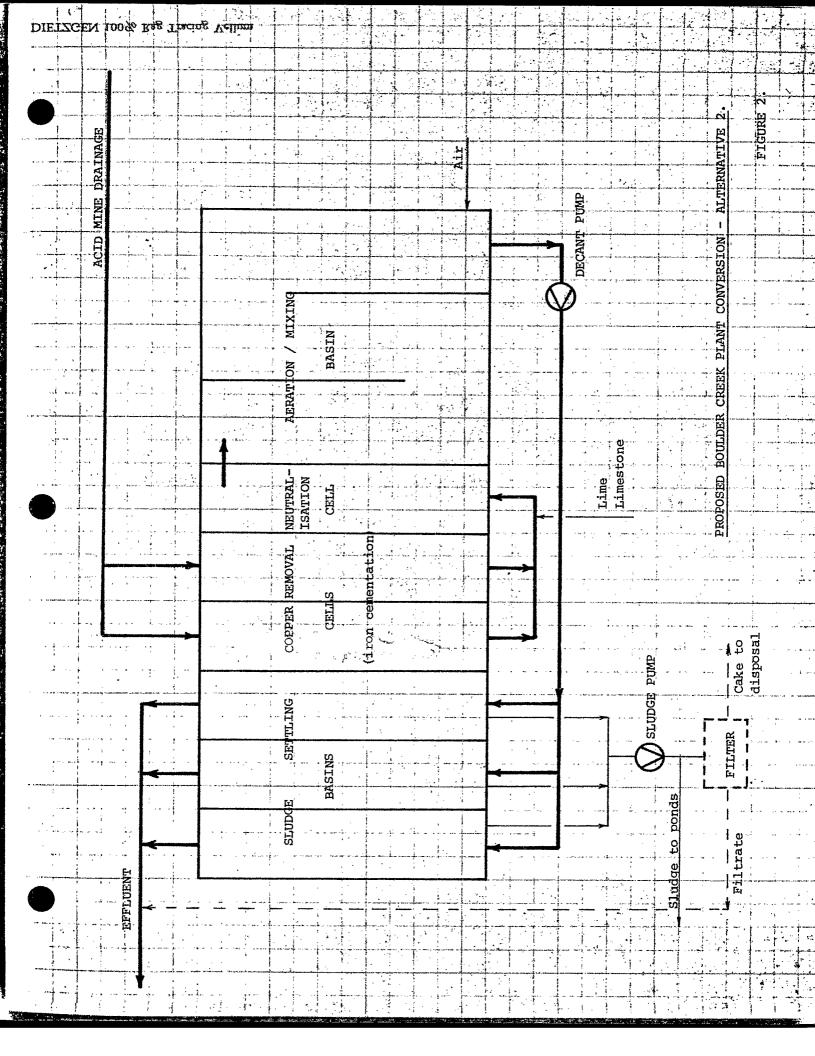
PROJECT SCHEDULE

The work proposed under cost items a) and b) will be performed as shown on the attached schedule. The recirculation of AMD into the mine would commence about two weeks after delivery of the equipment, and would continue for 2 months.

REFERENCES

- 1. Pierce, C. and R.N.Smith, 1971. General Chemistry workbook.
 4th Ed. Freeman & Co. N.Y. 368 pp.
- 2. Ross, L.W., 1973. Removal of Heavy Metals from Mine Drainage by Precipitation. EPA report EPA-670/2-73-080.
- 3. Bhattacharyya,D et al. 1981. Precipitation of Heavy Metals with Sodium Sulfide: Bench-Scale and Full-Scale Experimental Results. AIChE Symposium Series Paper 0065-8812-81-4714-0209.
- 4. Kim, B.M. 1981. Treatment of Metal Containing Wastewater with Calcium Sulfide. AIChE Symposium Series Paper 0065-8812-81-4842-0209.





PROJECT SCHEDULES

a) Pilot study

DE TARN 1864 - For Thomas Velous 12

ACTIVITY	Elapsed time from project approval (days)
Mobilisation/Equipt	
Set-up on site	
Pilot studies	
Data evaluation	
Report preparation	
Report submission	
Demobilisation	
Project completed	
b) Plant study	. 0 20 <u>4</u> 0 60 80 100

ACTIVITY		s	Elapsed	time	from	project	approval	(days)	.*	,	•
Plant alterations										S	
Rental equipment installation					•						* + 3 0 * * * * * * * * * * * * * * * * * * *
Plant-scale tests		, c			* 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ا المحادد المح المحادد المحادد المحاد					- ·
Data evaluation				ـــــ. ــــــر						•	
Report preparation	,	-		•	r	` .	-		-	· · ·	e - e
Report submission			e eget om				. 5		e Far		
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Project completed.		ž.		,	r		•				,•
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APPENDIX 5

ANALYTICAL RESULTS (Chemex Labs)

a) Slickrock Creek Plant

Water analysis

Assay equivalent

Ag <0.10 mg/l Au <0.01 mg/l

4 0.00035 oz/ton
4 0.000035 oz/ton

b) Boulder Creek Plant

Water analysis

Assay equivalent

Ag 0.10 mg/l Au 0.10 mg/l 0.00035 oz/ton 0.00035 oz/ton

c) Copper concentrate assay

Cu 58.3 %

Ag 28.1 g/ton Au 0.2 g/ton

Pd **4**0.1 g/ton

1.0 oz/ton 0.007 oz/ton <0.0035 oz/ton

Copper Studge vermoved from Soulke (veele cemulation plant. Pan Canadian Consultants Limited

1040 - 999 Suite 424 - 882 West Hastings Street Vancouver British Columbia WEENER V6C 1M3 (604) 688-8618

Environmental and engineering consultants to industry and government

RECEIVED A REGION IX

OCT 24 10 =0 AM *83



12 October 1983

United States Environmental Protection Agency Region IX 215 Fremont Street San Francisco, CA 94105 U.S.A.

Attn: Mr. Harry Seraydarian, Director, Toxics & Waste Management Division.

Dear Sir.

We were requested recently by Mr. C. N. Thodos, President of Ruskin Developments Ltd., to provide you with copies of data we had collected during the project work we undertook for Ruskin on the Iron Mountain property. Some of the paperwork in our files is not relevant to your investigation, so we have sorted out the information that may be useful.

The enclosures are:

- our final report to Ruskin (which contains much earlier data in the appendices)
- copies of chemical analyses on acid mine drainage, and on treated water samples (after our tests).

We do not possess any other information that would be useful to your investigation. We understand that Ruskin will be asking their geological consultant to forward data relating to the geology of the area.

Please confirm that you have received this information.

Yours truly

PAN CANADIAN CONSHLTANTS LIMITED

W. B. Alderton, P.Eng., "

President.



time.

test Itd.

1523 WEST 3rd AVENUE, VANCOUVER, B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

Report On	Analysis of solution samples	File No	1298F
Reported To	C. G. Environmental Engineering	P.O. #	
	5583 Spruce St.	Date	July 26, 1983
	Burnaby, B.C. V5G 1Y7		
Attention:	Dr. C. Guarnaschelli, P. Eng.		

We have tested the samples submitted by you on July 18, 1983 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled as given on the following Plasma Certificates.

METHOD OF TESTING:

Prior to analysis the samples were digested using an ultra pure nitric acid. The resulting solutions were then analyzed for metals using an Inductively Coupled Argon Plasma Spectrograph.

RESULTS OF TESTING:

See attached Plasma Certificate.

Republic

Supervisor

Trace Netals Laboratory

/cs



test Itd.

1523 WEST 3rd AVENUE. VANCOUVER. B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

To: C. G. Environmental Engineering

PLASMA SPECTROGRAPHIC ANALYSIS CERTIFICATE

5583 Spruce St.

Burnaby, B.C. V5G 1Y7

File No. 1298F

Date July 26/83

Attention:

Dr. C. Guarnaschelli, P. Eng.

Me hereby Certify that the following are the results of plasma spectrographic analysis made on solution samples submitted.

interig etting		10/Superna-	10/superna-	1/superna-	Compsite \	ppt 3.9	
Sample Identification		tant	tant		As veceved		
		3.2	3.9	4.2	' '		
Neutralised with	,				B 0	Cl. s. h	
NAOH to be	4	2.5	3.9	4.2	higuial	some los	
10011 10 91		3.6	- 1	7.6	Sample	bH 39.	Detection Limit
Aluminum	ΑI	742.	556.	594.	763.	2030.	1.5
Antimony	Sb	L	L	L	L	L	1.5
Arsenic	As	L	L	L	L	L	3.0
Barium	Ba	0.10	0.067	0.027	0.020	0.36	0.01
Beryllium	Be	L	L	L	L	L	0.03
Det ymum							
Bismuth	Bi	L	L	L	L	L	5.0
Boron	В	L	L	L	L	L	0.10
Cadmium	Cd	4.30	4.37	4.41	4.32	3.83	0.25
Calcium	Ca	132.	130.	131.	133.	117.	0.10
Chromium	Cr	L	L	L	L	L	0.30
Cobalt	Со	1.25	1.18	1.19	1.16	1.52	0.20
	Cu	129.	119.	119.	133.	189.	0.15
Copper	Fe	4850.	4230.	4530.	5510.	11800.	0.30
Iron	Pb	0.89	0.71	1.00	L.	5 1	0.80
Lead		413.	412.	421.	428.	382.	0.01
Magnesium	Mg	113.			,		
Manganese	Mn	12.6	12.6	12.8	12.9	11.1	0.03
Mercury	Hg	_	_	-	-	-	-
Molybdenum	Мо	L	L	L ·	L	L	0.40
Nickel	Ni	0.35	0.33	0.37			0.25
Phosphorus	P04	9.93	4.64	6.14	13.6	46.6	4.0
Potassium	K	60.1	60.5	60.1	`49.3	57.8	0.1
Selenium	Se	_	_	-	-	-	
Silicon	SiO ₂	134.	112.	117.	126.	225.	0.8
Silver	Ag	L	L	L	L	L	0.3
Sodium	Na	2310.	3320.	3240.	53.4	2910.	1.0
Strontium	Sr	0.20	0.21	0.22	0.18	0.25	0.01
Tin	Sn	L	L	L	L	L	0.30
Titanium	Ti	0.13	0.11	0.11			0.06
Tungsten	w	-	-	-	_	_	-
Uranium	U	-	-	_	· .	-	-
	v	1.19	0.39	0.50	1.23	5.98	0.10
Vanadium		606.	607.	626.	631.	561.	0.15
Zinc	Zn	300.		1	1	1 (7)	<u> </u>

All results expressed in parts per million.

L = less than.

Piasma 1

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T LTD.



can test Itd.

Report On	Analysis of solution samples	File No	0987F	
Penorted To	C. G. Environmental Engineering		0	
neported 10	5583 Spruce St.		June 20, 1983	
	Burnaby, B.C. V5G 1Y7			
Attention:	Dr. C. Guarnaschelli, P. Eng.			

We have tested the samples submitted by you on June 15, 1983 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled as given on the following Plasma Certificates.

METHOD OF TESTING:

Prior to analysis the samples were digested using an ultra pure nitric acid. The resulting solutions were then analyzed for metals using an Inductively Coupled Argon Plasma Spectrograph.

RESULTS OF TESTING:

See attached Plasma Certificate.

CAN TEST LTD

Richard S / Jornitz

Supervisør

Trace Metals Laboratory

/cs



1523 WEST 3rd AVENUE, VANCOUVER, B.C. V6J 1J8 • TELEPHONE (604) 734-7276 • TELEX 04-54210

C.	G.	Environmental	Engineering
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PLASMA SPECTROGRAPHIC **ANALYSIS CERTIFICATE**

5583 Spruce St.

File No. 0987F

Burnaby, B.C. V5G 1Y7

Date June 20/83

Attention:

To:

Dr. C. Guarnaschelli, P. Eng.

Me	hereby Certify	that the following are the results of plasma spectrographic analysis made or	solution	samples submitted.
•	~ =	·		

Sample Identification		Composite #1	Supernatant #1 pH 5.5	NaS Supernatant #2		
		Mixtue of Bulka o Sidwda	Newhalised Litt NaDH	Afta Nass alded.		Detection Limit
Aluminum Antimony Arsenic Barium Beryllium	Al Sb As Ba Be	674. L 13.0 L	4.48 L L 0.013 L	L L L 0.36		1.5 1.5 3.0 0.01 0.03
Bismuth Boron Cadmium Calcium Chromium	Bi B Cd Ca Cr	L 4.50 6.20 119. L	L L 5.18 106. L	L L L 57.4 L	,	5.0 0.10 0.25 0.10 0.30
Cobalt Copper Iron Lead Magnesium	Co Cu Fe Pb Mg	L 154. 7260. 2.50 394.	L 4.36 5180. L 346.	L 0.080 2120. L 185.		0.20 0.15 0.30 0.80 0.01
Manganese Mercury Molybdenum Nickel Phosphorus	Mn Hg Mo Ni PO ₄	11.4 - L 0.29 15.3	10.1 - L L 8.74	5.26 - L L L		0.03 - 0.40 0.25 4.0
Potassium Selenium Silicon Silver Sodium	K Se SiO ₂ Ag Na	29.4 - 129. L 31.6 ,	22.6 - 33.2 L 4140.	16.5 - 16.7 L 4400.		0.1 - 0.8 0.3 1.0
Strontium Tin Titanium Tungsten Uranium	Sr Sn Ti W U	0.13 L 1.14	0.19 L 0.12	0.10 L 0.13		0.01 0.30 2.5 -
Vanadium Zinc	V Zn	1.02 806.	L 598.	L 132.	551	0.10 0.15

All results expressed in parts per million.

L = less than.

Plasma 1

CAN TEST LTD.

Spectroscopist



ENVIRONMENTAL LABORATORY 2218 RAILROAD AVENUE, P.O. BOX 2088 REDDING, CA 96001—TELEPHONE (916) 243-5831 DATE 1 OF 2

Priysical Chemical & Bacteriological Analysis

SPECIFIC ANALYSIS

ATTN: Bill	AldertoN	D1 PHONE:		
		DATE RECEIVED		BY: <u>client</u>
TESTS	B in=Boulder Ck. Plant Influent	B lgry out=Boulder Plant Primary cell		t=Boulder Ck.Plant effluent
_{рН} (units)	1.20	1.33		1.33
Total Dissolved Solids	57720	59870		55320
Copper	166	13.6		5.17
Total Iron	11,300	13,100		13,200
Ferrous Iron	5160	6520		6670
Zinc	1050	1060	1050	52.3
Ferric Iron (by calculation)	6140	6580		6530
COMMENTS: Result	s are in milligrams p	per liter unless othe	rwise noted.	
	- Allen Control of the Control of th			

The information shown on this sheet is test data only and no analysis or interpretation is intended or implied.

Bacteriological, and Bioassay Examinations



ENVIRONMENTAL LABORATORY 2218 RAILROAD AVENUE, P.O. BOX 2088 REDDING, CA 96001-TELEPHONE (916) 243-5831 REF. NO. 9230DATE 6/21/83PAGE 2 OF 2

Physical Chemical & Bacteriological Analysis

SPECIFIC ANALYSIS

•				
	ng, Ca. 96001		PHONE:	
AMPLE DESCRIPTION _Iron Mountain Mine				
DATE OF SAMPLE	6/14/83	DATE RECEIVED		
TESTS		<u>S in=Slickrock Ck.</u> plant influent	S out=Slickrock Ck. plant effluent	
pH (units)		2.59	2.62	
Total Dissolved		10490 [•]	10130	
Solids Copper		122	122	
Total Iron		1210	1230	
Ferrous Iron		477	474	
Zinc		49.1	50.0	
Ferric Iron		733	756	
(by calculation)				
COMMENTS: Results	are in mill:	igrams per liter unless oth	nerwise noted.	

Bacteriological, and Bioassay Examinations

The information shown on this sheet is test data only

State Approved Water Laboratory for Chemical,

The information shown on this sheet is test data only and no analysis or interpretation is intended or implied.